

ANTIBIOCORROSIVE HYBRID MATERIALS WITH HIGH DURABILITY

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Abstract. We have developed novel antibiocratic hybrid materials based on functionalized perfluoroalkyl methacrylate copolymers with epoxy groups in main chains and selected biologically active compounds. The hybrids are transparent, show good adhesion to various surfaces (plastic, wood), high viscoelastic recovery in scratch testing, low wear rates and glass transitions above 323 K. No phase separation is seen in scanning electron micrography. Enhanced mechanical strength and good abrasion resistance are advantages for uses of our protective and antibiocratic coatings in various applications including protection of cultural heritage.

Keywords: hybrid materials, protective coatings, antibiocratic coatings, perfluoroalkyl methacrylates.

1. Introduction

Microbial pollutants cause damage to natural and synthetic polymeric materials and wares as well as to objects of cultural heritage and to ecosystem. This situation behooves us to develop materials and methods that can effectively prevent and/or inhibit the growth of detrimental microorganisms and to control biocorrosion processes [1, 2].

During the last two decades, design of the polyfunctional hybrid materials has attracted considerable research interest. The wide range of possible hybrids may include innovative combinations, starting from organic and organometallic molecules to biomolecules, inorganic clusters, fullerenes or nano- and submicro sized particles dispersed in polymer matrix. Functionalized polymeric hybrids with a variety of structures have a wide range of applications including antimicrobial polymer composites, adhesives, dye composites, optical materials, membranes, biomedical materials, coatings, and more [3-5]. Polyfunctional polymers with linear macrochains and regular structure, containing Si–N–, Si–O and NH groups can be used to obtain bioactive composites with specific properties – including important antibiocratic capability [6, 7]. Among them are polyfunctional heterochain organic polymers (polyurethane elastomers, polyurethane-acrylates, polyurethane ionomers and more), carbofunctional silicon-organic and other polyfunctional heterochain polymers [8].

Fluorinated polymers and copolymers display high thermal stability, satisfactory mechanical properties at high temperatures, resistance to oxidation and hydrolytic decompositions, weatherability, low flammability, inertness to solvents (hydrocarbons, acids, and alkalis), low dielectric constants and low surface energies [9-15]. Due to such unique combination of advantageous properties, fluoropolymers are widely used in architectural, optoelectronic, automotive, aerospace, and aeronautic industries, microelectronics, and chemical engineering as well as in medicine, such as dental materials and artificial joints. The low refractive index and high optical transparency make amorphous perfluoropolymers a promising candidate for applications in high-performance protecting coatings, surface modifiers, and optical materials or shatter-resistant alternative to glass [10, 16, 17].

Despite such unique properties of fluorine-organic polymers, they have worse adhesion properties than epoxy-based polymeric matrices and coatings.

Abovementioned considerations led to the creation of our program of work. The main objective of our work was to choose relatively easily available perfluoroalkyl methacrylates (F_nMA) with good reactivity as initial

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monomers for synthesis of hydrophobic and mechanically stable fluorine-organic polymers. By copolymerization of selected perfluoroalkyl methacrylates with allyl glycidyl ether (epoxy allyl monomer) containing adhesive functional groups makes it possible to functionalize transparent fluorine-organic methacrylates by incorporation of easily hardened epoxy groups in their macro chain.

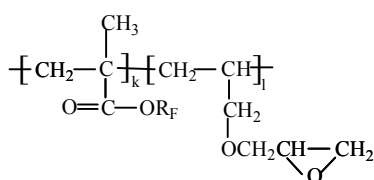
The most novel aspect of the presented work is the development of easily curable polymer matrices for antimicrobial coatings based on fluorine-organic methacrylates with an epoxy group and regular structure instead of the previously used by us polyepoxides [18] which are used as blends modified by silicon-organic oligomers which complicates the reproducibility of the properties of resulting materials and makes the composition more expensive.

2. Experimental

2.1. Synthesis

Despite the unique properties of fluoropolymers, they are characterized by worse adhesion properties compared to other polymers such as polyurethanes or polyepoxides used in antibio-corrosive matrices [18, 19]. This factor had to be kept in mind in our synthesis.

New hydrophobic and mechanically stable fluorine-organic polymers were obtained by means of targeted functionalization of polyperfluoroalkyl methacrylates (F_n MAs). Radical copolymerization of selected fluorine containing monomers with allyl glycidyl ether was carried out to obtain copolymers with fluoroalkyl- and epoxy side groups in their main chain (Scheme 1):



$R_F = -\text{CH}_2-(\text{CF}_2)_m\text{H}$; $m=2, 4, 5$; $k+l = n$ (average degree of copolymerization)

Scheme 1. Functionalized polyperfluoroalkyl methacrylates

Based on preliminary investigations, co-monomers with the molar ratios of 1:1 and 7:3 were chosen. The reaction was carried out in a polydimethylsiloxane (PMS-100) oil bath in the presence of 1 wt% of benzoyl peroxide (BPO, initiator). The mixture was heated to 343–358 K in dry argon area during 4–5 h, in each case until formation of a highly viscous transparent mass – a solution of copolymers in the corresponding monomers.

The obtained copolymers were isolated from reaction mixture by heptane from an ethyl acetate solu-

tion. The yield of copolymers was 70–80 %. The specific viscosity (η_s) of the copolymers determined in the capillary viscosimeter in 1% ethyl acetate solution was in the range of 0.15–0.38 dL/g. 1,1,3-Trihydrotetrafluoropropyl methacrylate (F_4 MA) formed solid, rigid products; copolymers based on 1,1,5-trihydrooctafluoropropyl methacrylate (F_8 MA) and 1,1,7-trihydrododecafluoropropyl methacrylate (F_{12} MA) formed elastic transparent solid products.

The formation of comparatively low molecular weight copolymers should be associated with the degradative effect of radical mechanism of copolymerization caused by high mobility of C-H groups bonded to the allyl monomer's oxygen [20]. By determination of the epoxy numbers, it was established that the content of allyl glycidyl ether rings in the copolymers was less than 20 mol%.

Fourier transform infrared spectroscopy (FTIR) was performed with a Perkin Elmer FT-IR Spectrum BX 11 ($350\text{--}4000\text{ cm}^{-1}$) spectrophotometer in KBr monocrystal. In the infrared spectra weak absorption bands characteristic of the epoxy group are shown at 830, 915–925 and $1245\text{--}1262\text{ cm}^{-1}$. Absorption band for ester carbonyl group appears at $1739\text{--}1750\text{ cm}^{-1}$ and for carbonyl (C=O) groups at $1633\text{--}1665\text{ cm}^{-1}$. The bands at $3000\text{--}3002$ and $1370\text{--}1410\text{ cm}^{-1}$ are attributed to the alkyl (CH_3) groups and the CH_2 , C-H and C-F bands appear at $2905\text{--}2910$ and $1070\text{--}1230\text{ cm}^{-1}$.

As bioactive component we chose α -ferrocenylethyl-4-methoxy-2-nitrophenylamine, α -ferrocenylethyl-4-(1-adamantoyl)-2-nitrophenylamine] and heterometal coordination compounds containing organometallic [bis(η^5 -cyclopentadienyl)iron] and polycarbocyclic fragments (tricyclo-[3.3.1.1^{3,7}]-decane) [18, 21] (Table 1, Scheme 2). Sady and coworkers have developed a measure of antimicrobial activity which they called "Pa" [16]. To avoid confusion with the Pascal unit, we shall use the term "Aa" for antibacterial activity they defined. Aa against *influenza*, *picornavirus*, *adenovirus* and *poxvirus*) is in the range of $Aa \approx 0.601\text{--}0.778$. For antiparasitic activity against *coccidial*, *histomonas* and *nematodes* we have the of range $Aa \approx 0.536\text{--}0.689$. For antimycobacterial activity we have $Aa \approx 0.549\text{--}0.599$. Apparently for $Aa > 0.5$ "the given compound will most likely exhibit this activity in experiment" [22].

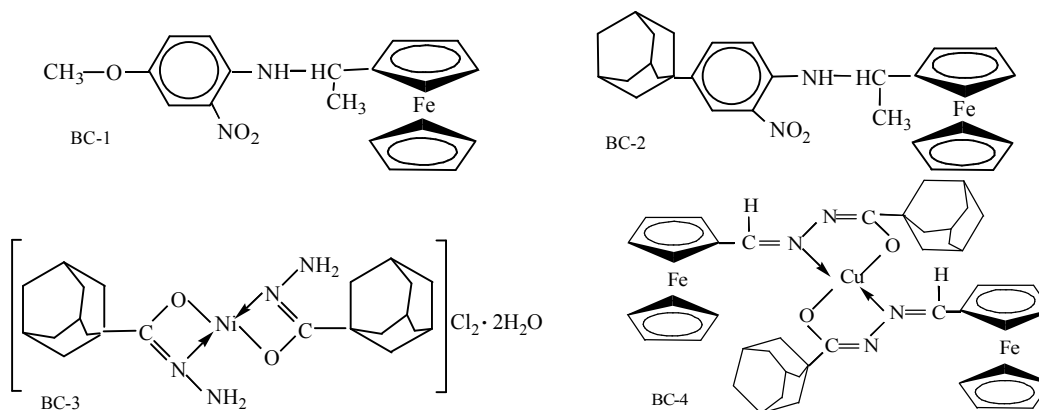
Taking into account the accessibility and diversity of polymeric and bioactive components for the design of targeted materials, one finds a great opportunity for varying of combinations; during their creation, the main idea is to achieve prolonged maintenance of their appearance and improvement of tribological, mechanical and other operational characteristics.

Antimicrobial hybrid materials were prepared by adding of 3 wt% of selected bioactive compounds (BC)

into the obtained functionalized polyperfluoroalkyl methacrylates (F_n MA-AGE/1:1, 7:3). The components were stirred for 30–40 min (343 K), then hexamethylenediamine (HMDA; 5, 7, 10 wt%) was used

as a curing agent. The resulting light-colored homogenous composites were deposited on the surfaces of various materials and kept for 3–5 days at room temperature.

The materials so obtained are listed in Table 1.



Scheme 2. Bioactive hybrid components based on organometallic and polycarbocyclic fragments

Table 1

Antimicrobial composites based on copolymers with fluoroalkyl and epoxy side groups

Number	Composite	Number	Composite
I	F_4 MA-AGE (1:1) / 5% HMDA	XVIII	F_8 MA-AGE (1:1) / 3% BC-3 / 7% HMDA
II	F_4 MA-AGE (1:1) / 3% BC-1 / 5% HMDA	XIX	F_8 MA-AGE (1:1) / 3% BC-4 / 7% HMDA
III	F_4 MA-AGE (1:1) / 3% BC-2 / 5% HMDA	XX	F_8 MA-AGE (1:1) / 10% HMDA
IV	F_4 MA-AGE (1:1) / 3% BC-3 / 5% HMDA	XXI	F_8 MA-AGE (1:1) / 3% BC-3 / 10% HMDA
V	F_4 MA-AGE (1:1) / 3% BC-4 / 5% HMDA	XXII	F_8 MA-AGE (7:3) / 7% HMDA
VI	F_4 MA-AGE (1:1) / 7% HMDA	XXIII	F_8 MA-AGE (7:3) / 3% BC-1 / 7% HMDA
VII	F_4 MA-AGE (1:1) / 3% BC-1 / 7% HMDA	XXIV	F_8 MA-AGE (7:3) / 3% BC-2 / 7% HMDA
VIII	F_4 MA-AGE (1:1) / 3% BC-3 / 7% HMDA	XXV	F_8 MA-AGE (7:3) / 3% BC-3 / 7% HMDA
IX	F_4 MA-AGE (1:1) / 10% HMDA	XXVI	F_8 MA-AGE (7:3) / 3% BC-4 / 7% HMDA
X	F_4 MA-AGE (1:1) / 3% BC-3 / 10% HMDA	XXVII	F_8 MA-AGE (7:3) / 10% HMDA
XI	F_4 MA-AGE (7:3) / 7% HMDA	XXVIII	F_8 MA-AGE (7:3) / 3% BC-3 / 10% HMDA
XII	F_4 MA-AGE (7:3) / 3% BC-3 / 7% HMDA	XXIX	F_{12} MA-AGE (1:1) / 7% HMDA
XIII	F_4 MA-AGE (7:3) / 10% HMDA	XXX	F_{12} MA-AGE (1:1) / 3% BC-1 / 7% HMDA
XIV	F_4 MA-AGE (7:3) / 3% BC-3 / 10% HMDA	XXXI	F_{12} MA-AGE (1:1) / 3% BC-2 / 7% HMDA
XV	F_8 MA-AGE (1:1) / 7% HMDA	XXXII	F_{12} MA-AGE (1:1) / 3% BC-3 / 7% HMDA
XVI	F_8 MA-AGE (1:1) / 3% BC-1 / 7% HMDA	XXXIII	F_{12} MA-AGE (1:1) / 3% BC-4 / 7% HMDA
XVII	F_8 MA-AGE (1:1) / 3% BC-2 / 7% HMDA		

2.2. Thermophysical Characterization

Thermophysical properties of our hybrid samples were studied with differential scanning calorimetry (DSC) and thermogravimetry (TGA). DSC tests were performed with a differential scanning calorimeter from Netzsch, Selb, Germany, model DSC 200, to locate the phase transitions. Testing conditions were as follows: temperature range from 173 up to 573 K and heating rate of 5 K/min in dry N_2 atmosphere. Samples of about 10 mg each were enclosed in aluminium DSC capsules.

Perkin Elmer TGA7 apparatus was used in order to evaluate thermal stability and degradation behavior of

each sample. Tests were conducted under dry N_2 atmosphere in the temperature range of 323–1073 K and at the heating rate of 10 K/min. Both DSC and TGA techniques are well explained by Menard [23]. DSC monitors heat effects associated with phase transitions and chemical reactions as a function of temperature and is used to characterize properties such as the crystallinity, thermal transitions and the melting temperatures.

2.3. Scratch Resistance Testing

Scratch and adhesion tests were performed using a Micro-Scratch Tester (MST) from CSM, Peseux, Neucha-

tel, Switzerland, utilizing the CSEM Scratch Software Version 2.3; one applies a constantly increasing force from 0 to 30.0 N to the samples or else a constant force.

The sliding wear determination (SWD) was performed by multiple scratching with a diamond tip along the same groove [24, 25]. Two parameters are obtained in the determination of scratch resistance: penetration (instantaneous) depth R_p and residual (healing) depth R_h determined two minutes later. The viscoelastic recovery (φ , %) is defined as:

$$\varphi = [(R_p - R_h)/R_p] \cdot 100 \quad (1)$$

Progressive scratch testing was performed with the following parameters: initial load 0.03 N, final load 30.0 N, loading rate 30.0 N/min, scanning load 0.03 N, scratch length 8.0 mm and scratch speed 5.9 mm/min. SWD tests were performed under a constant load of 5.0 N with the scratch length 5.0 mm. For each sample 10 scratch runs were performed, at the scratch velocity 10.0 mm/min at room temperature (293 ± 2 K). The conical diamond indenter with 200 μm diameter and the cone angle of 120° was used.

2.4. Dynamic Friction

Dynamic friction λ was determined by sliding using a Nanovea pin-on-disk tribometer from Micro Photonics Inc. 440 steel balls made by Salem Speciality Balls with the diameter of 3.2 mm were used. The tests were performed under the following conditions: temperature 293 ± 2 K, speed 100 rpm, sliding distance 40 m, radius 2.0 mm, load 5.0 N, number of revolutions 2000, and test duration 20 min. The friction is defined as:

$$\lambda = f / F_n \quad (2)$$

where f is the friction force in Newtons; F_n is the normal force.

3. Results and Discussion

3.1. Thermophysical Characterization

Our DSC results show that all our materials are amorphous. Melting transitions are not visible and exothermic peaks characteristic of crystallization are not

displayed. Kalogeras and Hagg Lobland note that the glass transitions regions are usually broad [26]. There is a habit of representing those regions by a single number called the glass transition temperatures of tested samples (T_g) and there are various ways defining that temperature. We have taken the values of T_g as the middle points of the falls of the DSC curves. All hybrids have T_g points in the region of 323 K to 338 K, which is important for the applications of our coatings. DSC diagrams show also phase transitions in the glassy state – so called α -transitions – centered in the range from 240 K to 230 K (Table 2). Addition of bioactive compounds enhances the stability of the low temperature amorphous phase.

TGA was used to evaluate thermal degradation behavior of our hybrids. Thermal stability parameters: temperature of destruction (T_{des}), weight loss (%) and the temperature of maximum rate of degradation (T_{max} ; temperature after no changes are observed) are displayed in Table 3.

We see that polymer composites and antimicrobial hybrid materials, containing fluoroalkyl- and epoxy side groups obtained by radical copolymerization of 1,1,3-trihydrotetrafluoropropyl methacrylate with AGE, are stable up to 693 K; the respective weight loss in the range of 693–728 K is 25–37 % (Table 2, I–XIV).

As also seen in Table 2, increasing the fluoroalkyl chain length improves the resistance to thermal degradation of the hybrids. Our materials containing fluoroalkyl- and epoxy side groups obtained by radical copolymerization of 1,1,5-trihydrooctafluoropropyl methacrylate with AGE (F_8 MA-AGE) are stable up to 713 K and weight loss in the range of 713–728 K consists of 18–30 % (Table 2, XV–XXVIII). The hybrids based on 1,1,7-trihydrododecafluoropropyl methacrylate (F_{12} MA-AGE) are stable up to 703 K and weight loss in the range of 705–710 K consists of 29–37 % (Table 2, XXIX–XXXVII).

We infer that modification increases the thermal stability of our materials and weight loss is shifted to higher temperatures; these effects are enhanced further by addition of bioactive component and by increasing the curing agent content.

Table 2

T_g/T_a values obtained for some hybrid materials containing perfluoroalkyl methacrylic and epoxy side groups

Hybrid	T_g/T_a , K	Hybrid	T_g/T_a , K	Hybrid	T_g/T_a , K
I	337.7/230.6	VIII	329.0/238.5	XVIII	327.1/241.1
II	333.3/232.5	X	332.7/237.2	XXV	325.5/239.8
IV	334.7/230.4	XII	331.7/234.1	XXVIII	327.4/237.6
VII	335.6/233.5	XVI	328.2/239.4	XXXIII	328.0/230.7

TGA data for polymer composites and antimicrobial hybrid materials containing perfluoroalkyl methacrylic and epoxy side groups

Hybrid composite	T _{des.} , °C	Weight loss, %	T _{max} , °C	Hybrid composite	T _{des.} , °C	Weight loss, %	T _{max} , °C
I	438	25	440	XVIII	439	27	440
II	433	37	435	XIX	432	29	435
III	440	34	445	XX	446	27	450
IV	440	24	445	XXI	441	17	445
V	428	37	430	XXII	435	30	440
VI	441	30	445	XXIV	446	30	450
VII	445	34	448	XXV	434	26	440
VIII	443	26	445	XXVII	453	26	455
IX	453	28	455	XXVIII	436	26	440
X	453	33	455	XXIX	432	37	435
XI	434	31	435	XXX	435	32	439
XIII	442	26	445	XXXI	436	28	440
XIV	418	33	420	XXXII	434	24	435
XV	439	28	440	XXXIII	437	31	440

3.2. Scratch Resistance Testing

Results of SWD are shown in Fig. 1 (penetration depths) and Fig. 2 (residual depths). Tribological properties of composites based on main polymer matrices were examined as a reference.

As one can see in Fig. 1, modification improves resistance of composites to instantaneous deformation by micro scratching. At the applied load, hybrid composites based on F₄MA-AGE = 1:1 (Fig. 1; II, III, V) have the original penetration depth in the range 98–110 μm while $R_p \approx 123$ μm for the basic polymer matrix. The increase of curing agent (HMDA) concentration from 5 to 7 and then to 10 wt% also causes improvement of penetration depth values of the basic polymer matrix on the average from 123 to 64 and to 59 μm, respectively (Fig. 1d; I, VI, IX).

Looking for the best material, we see that the maximum decrease of R_p value and the best resistance to instantaneous deformation is seen in the polymer matrix F₄MA-AGE 1:1/10 wt% HMDA and the hybrid composite based on it (Fig. 1; IX-X).

Diagrams of the penetration depths for materials based on F₈MA (Fig. 1; XV-XXI) also show improvement of resistance to instantaneous deformation (Fig. 1; XV, XX) along with increasing concentration of the curing agent (HMDA) from 7 to 10 wt%.

The increase of molar ratio of 1,1,3-trihydroxytetrafluoropropyl methacrylate in the copolymer (F₄MA-AGE = 7:3) is counterproductive for our purposes since we get larger values of the penetration depth (Fig. 1; XIII-XIV) comparatively to the matrices with a similar composition (Fig. 1; IX-X). Nevertheless, comparison of

composites - F₄MA-AGE 1:1/5 wt% HMDA and F₄MA-AGE 7:3/10 wt% HMDA show better resistance to instantaneous deformation by micro scratching for the latter one (Fig. 1; I, XIII).

In all cases, as it was expected, one observes typically a slight increase (on the average by 10–25 μm) of penetration depth by incorporation of BCs in polymer matrices. These effects can be explained by the spatial structures of BCs used (Fig. 1; VII, VIII, X, XIV; XVI-XIX, XXI).

Among the basic polymer matrices obtained based on F₄MA and F₈MA, the largest reduction in R_p displays the composite F₄MA-AGE 1:1/10 wt% HMDA (Fig. 1; IX). Comparison of testing results of hybrids with similar compositions shows shallow R_p values for matrices based on fluoromethacrylic copolymers with short fluoroalkyl chains (Fig. 1; XI, XV, XIII, XX, respectively).

Fig. 2 shows the residual (after healing) depth (R_h) diagrams for our composites at a constant load (5.0 N) as a function of the scratch test number. Residual depth of hybrids based on F₄MA largely decreases (Fig. 2; II, III, V). After some initial increases of R_h with the increasing test number, asymptotic behavior is seen; further runs provide hardly any change. The increase of concentration of the curing agent (HMDA) lowers residual depth of the basic polymer matrix (F₄MA-AGE 1:1) from 71 to 43 and 30 μm, respectively (Fig. 2; I, VI, IX). Incorporation of BCs into composites causes an insignificant decrease of R_h , on the average by 8–15 μm (Fig. 2; VII, VIII, X). The largest reduction of R_h is obtained by increasing the molar ratio of copolymers, namely for F₄MA-AGE = 7:3 (Fig. 2; XIII).

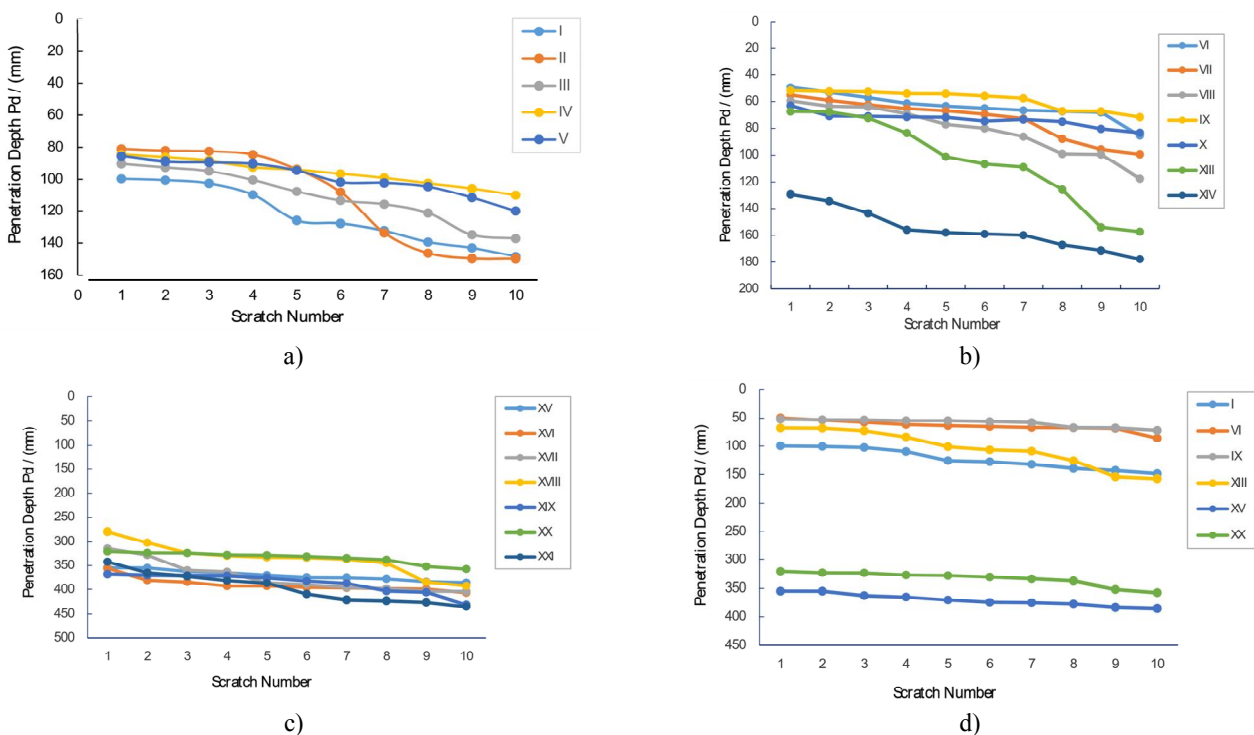


Fig. 1. Penetration depths of polymeric matrices and hybrid composites based on them: hybrid composites containing F₄MA-AGE (1:1 / 7:3) (a, b); hybrid composites containing F₈MA-AGE (1:1 / 7:3) (c) and comparison of penetration depths for hybrid composites containing F₄MA-AGE & F₈MA-AGE (1:1 / 7:3) (d)

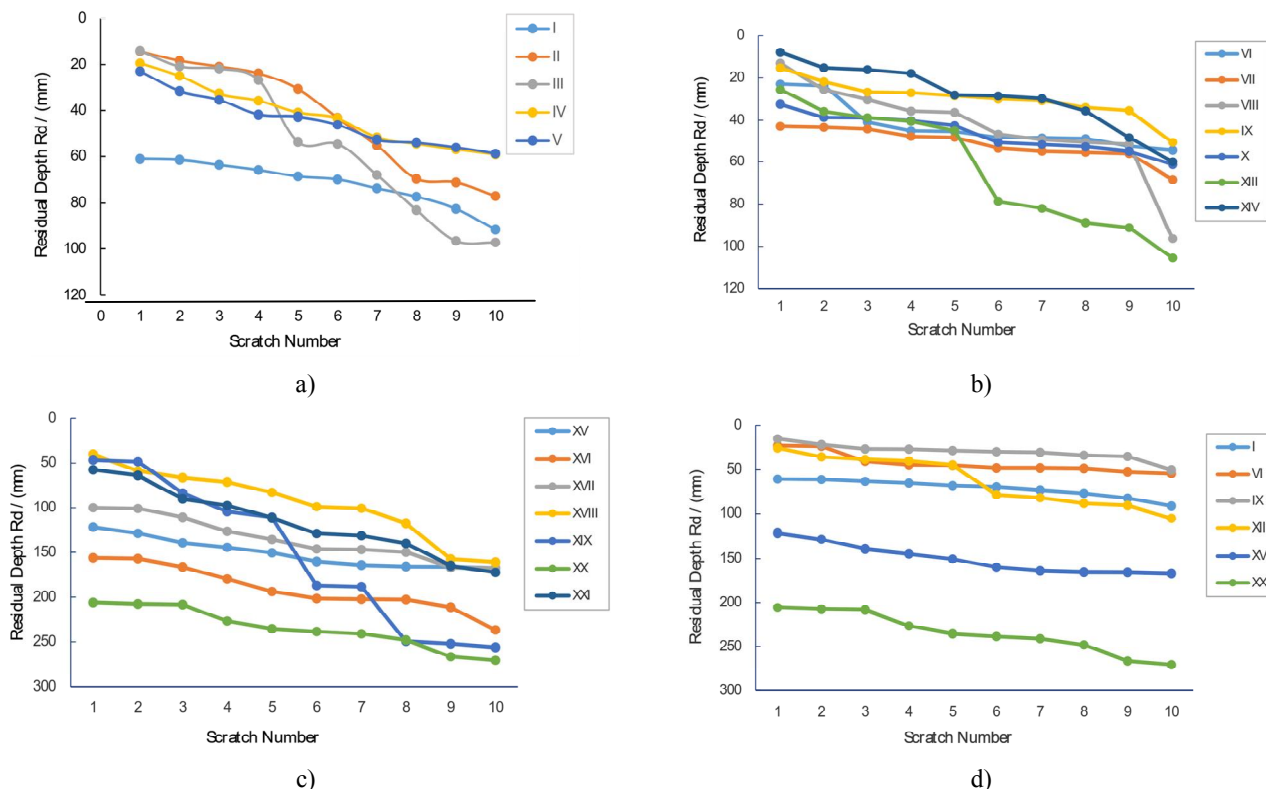


Fig. 2. Residual depths of polymeric matrices and hybrid composites based on them: hybrid composites containing F₄MA-AGE (1:1 / 7:3) (a, b); hybrid composites containing F₈MA-AGE (1:1 / 7:3) (c) and comparison of penetration depths hybrid composites containing F₄MA-AGE & F₈MA-AGE (1:1 / 7:3) (d)

We see that modification with bioactive components provides lowering of the residual depth of hybrid composites based on 1,1,5-trihydrooctafluoropropyl methacrylate (Fig. 2; XVII, XVIII, XXI). Comparison of the results for polymer matrices containing fluoroalkyl and epoxy side groups (F_4 MA-AGE & F_8 MA-AGE) shows a significant decrease of residual depths due to increasing concentration of the curing agent (Fig. 2; I, VI, IX). An increase of fluoroalkyl chain length of methacrylic copolymers, using polymer matrices with the same composition, causes a significant increase of R_h values (Fig. 2; VI and XV, IX and XX, respectively). Among the tested matrices the shallowest R_h is seen for the polymer matrix F_4 MA-AGE 1:1/10 wt. % HMDA (Fig. 2; IX).

Significant improvement in viscoelastic recovery of modified hybrid materials is seen as well (Fig. 3). The values of ϕ calculated from Eq. (1) are in the range between 53 and 97 %.

For composites obtained based on F_4 MA-AGE (equimolar ratio) the viscoelastic recovery is reduced by increasing curing agent content from 5 to 7 and then to 10 wt% (Fig. 3; I, VI, IX). For the polymer composites with otherwise the same composition, the value of ϕ is increased on the average by 30–40 % along with increasing

the molar ratio of fluoroalkyl methacrylic copolymers (Fig. 3; VI-VIII, XIV). For composites based on F_8 MA-AGE we see the higher viscoelastic recovery for composites with a lower content of curing agent (Fig. 3; XV, XX). Further modification with BCs improves the recovery behavior of scratched surfaces (Fig. 3; XVII-XIX, XXI).

Thus, viscoelastic recovery of our composites is significantly improved by increasing the fluoroalkyl chain length and molar ratio of corresponding methacrylic copolymers (Fig. 3; VI, XV). As expected, the scratch resistance and recovery are related to the local molecular structure, in particular to the intrachain bonds (primary interactions) of the segments on the scratching path.

We note that the sliding wear determination results were the basis for formulating an equation for the polymer brittleness B [25, 27], namely:

$$B = 1/[\varepsilon_b E'] \quad (3)$$

where ε_b is the tensile elongation at break at a given temperature T ; E' is the storage modulus at the same temperature obtained by dynamic mechanical analysis (DMA, see [25]); B for polymers is related to the viscoelastic recovery ϕ defined by Eq. (1), namely [27]:

$$\phi = 30.6 + 67.1e^{-B/0.505} \quad (4)$$

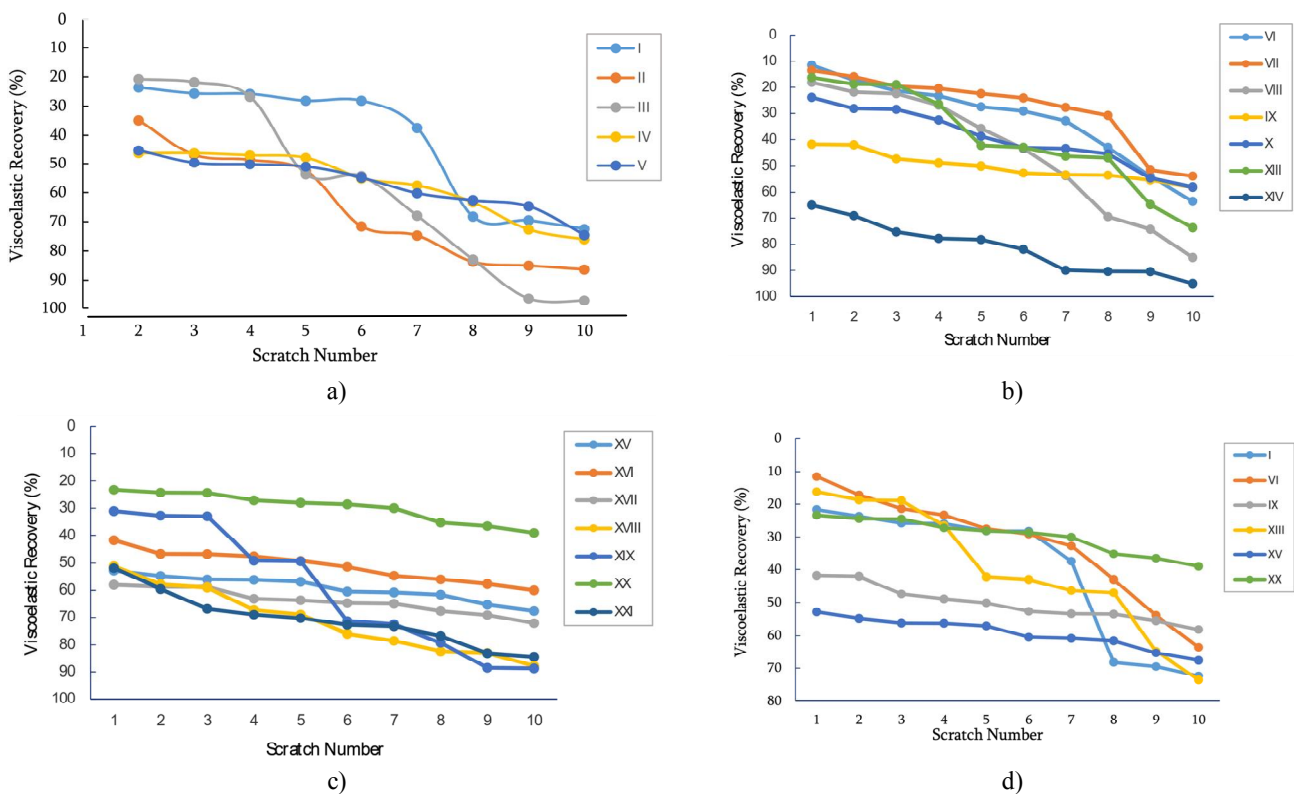


Fig. 3. Viscoelastic recovery of polymer matrices and hybrid composites based on them: hybrid composites containing F_4 MA-AGE (1:1 / 7:3) (a, b); hybrid composites containing F_8 MA-AGE (1:1 / 7:3) (c); and comparison of penetration depths for hybrid composites containing F_4 MA-AGE and F_8 MA-AGE (1:1 / 7:3) (d)

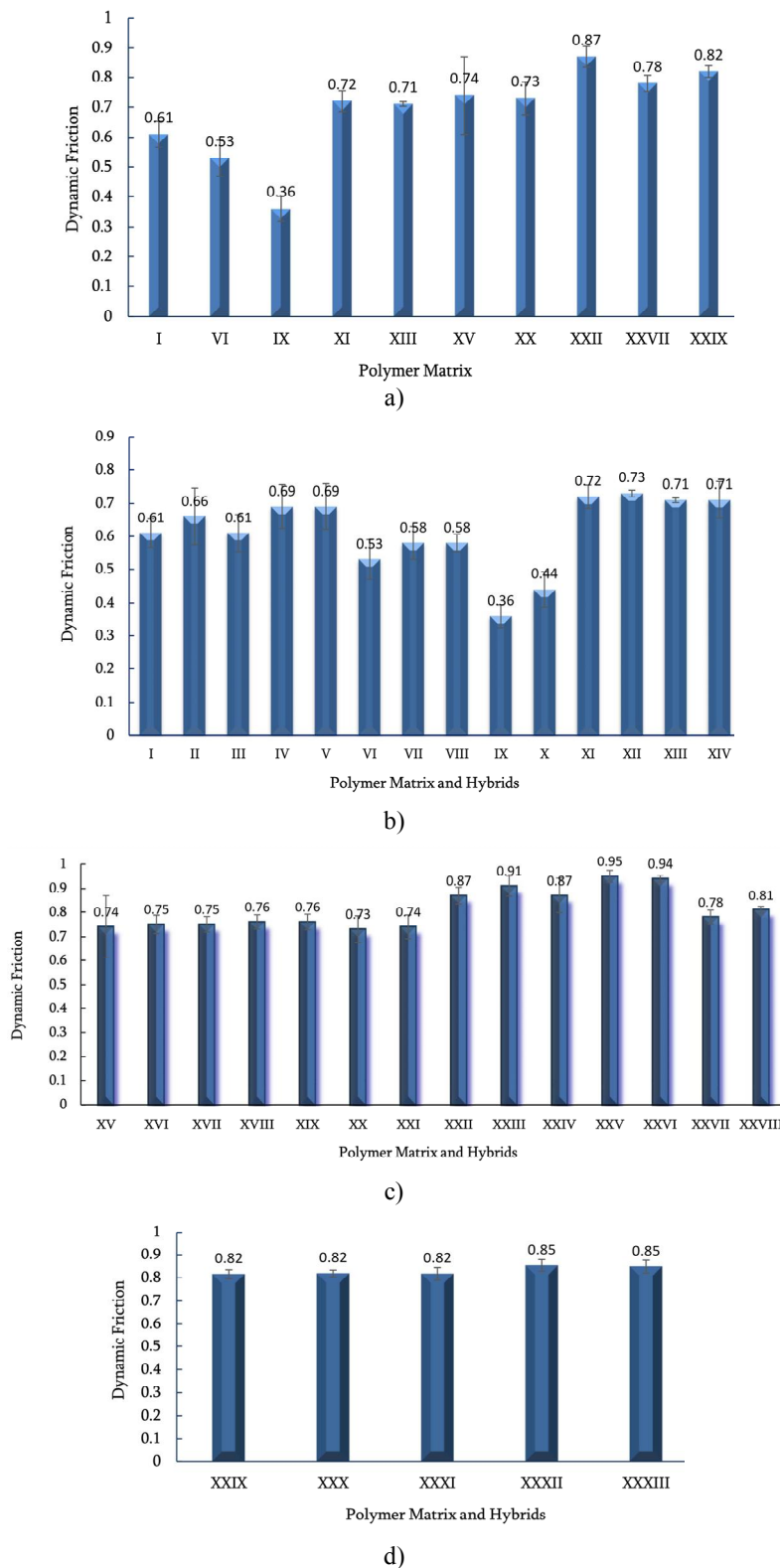


Fig. 4. Dynamic friction values of polymer matrices containing perfluoroalkyl methacrylic and epoxy side groups and hybrid composites based on them: results for polymer matrices (F₄MA-AGE, F₈MA-AGE and F₁₂MA-AGE; 1:1 / 7:3) (a); hybrid composites containing F₄MA-AGE (1:1 / 7:3) (b); hybrid composites containing F₈MA-AGE (1:1 / 7:3) (c); and hybrid composites containing F₁₂MA-AGE (1:1) (d)

3.3. Dynamic Friction Results

Qualitatively, friction is defined as the resistance to relative motion between two bodies in contact [25]. Static friction pertains to starting the motion, dynamic to maintaining it at a constant velocity. In many cases, we are interested in low friction values; not always since high friction provides high ballistic penetration resistance. Fig. 4 shows selected results obtained.

Dynamic friction as a function of composition of tested hybrids largely decreases when increasing the curing agent content (Fig. 4; I/VI/IX; XXII/XXVII, respectively). Insignificant reduction of dynamic friction is observed for composites XI/XIII and XV/XX. The increase of molar ratio of methacrylic copolymers causes substantial increase of the friction values for composites with similar compositions (Fig. 4; VI/XI; IX/XIII; XV/XXII; respectively). Meanwhile, the increase of fluoroalkyl chain length in the composites with similar compositions show the increase of the friction values of corresponding samples (Fig. 4; VI, XV and XXIX).

Comparison of average dynamic friction values of polymer composites based on F₄MA/F₈MA/F₁₂MA-AGE (1:1) and corresponding hybrids obtained by their further modification with BCs show insignificant increases (Fig. 4; XXIII-XXVI, XXVIII, XXX-XXXIII). The lowest dynamic friction is seen for the composite F₈MA-AGE 1:1/10 wt% HMDA (Fig. 4; XX and XXI). Small changes of dynamic friction for hybrids with similar compositions are not important for the application; consider the methacrylic copolymer (F₄MA-AGE = 7:3) with either 7 or 10 % HMDA (Fig. 4; XII and XIV).

Relatively high dynamic friction values are seen for the matrices based on the copolymer with the longest fluoroalkyl chain (F₁₂MA). We recall here the Bump Model developed in [28]. In friction testing the pin (indenter) does not move continuously along the surface but rather jumps from bump to bump. Composite IX in Figure 4 shows the lowest friction value of all. Its composition is F₄MA-AGE 1:1/10 % HMDA. Apparently HDMA provides small bumps. The highest value of λ is seen for F₈MA-AGE 7:3/3 % BC-3/7 % HMDA. Two factors seem to contribute to that highest λ value. First, as we see in Scheme 2, BC-3 has an unusually complicated three-dimensional structure, providing large obstacles to the indenter movement. Second, F₈MA-AGE has twice as long polymeric chain as F₄MA-AGE, providing larger bumps. In F₁₂MA-AGE reversals of fluoroalkyl chain directions are possible, providing smaller obstacles to the indenter movement.

3.4. Surface Morphology Observations

SEM observations of surface microstructures of our composites after tribological tests are displayed in Fig. 5.

The wear tracks for hybrids based on equimolar ratio of copolymers (F₄MA/F₈MA-AGE) and 10 wt % of curing agent are insignificant (Fig. 5; X and XXI). The increase of molar ratio of copolymers makes the wear tracks slightly more visible when compared to the hybrids with equimolar content of copolymers (Fig. 5; X/XIV; XXI/XXVIII, respectively). Composite XXVIII shows wear debris, and in optical image of the longest fluoroalkyl chain copolymer (F₁₂MA) wear debris with crack formation is observed (Fig. 5; XXXII).

By comparison of surface microstructures of tested materials based on various copolymers having similar composition, better scratch and wear resistance is shown for the polymer composites and hybrids containing the shortest fluoroalkyl methacrylic chain copolymer (F₄MA).

Thus, observations of surface microstructures are in agreement with our tribology results. Wear resistance is determined by the structure of used perfluoroalkyl methacrylates, by molar ratio of copolymers and by composition of targeted hybrid composites.

3.5. Aging and Weatherability

Aging tests at 313 and 333 K in the air were performed to determine weatherability (*complex action of moisture, air oxygen, carbon dioxide, and visible light*) of our hybrids. For six months all samples maintained their initial appearance, color, optical transparency and mechanical properties (surface homogeneity without splits formation).

Moisture medium affects the rate of microbial attachment and microbe dissemination on materials surfaces. Thus, hydrophobic properties of coatings play significant role in the process of adhesion of microorganisms on various surfaces.

The water absorption ability was determined by the gravimetric method described by Travinskaja and colleagues [29]. The water absorption ΔW can be calculated as:

$$\Delta W = [(M_S - M_D)/M_S] \cdot 100\% \quad (5)$$

where M_S is the mass of the material saturated with water; M_D is the mass of the dry material.

We have found that the water absorption of our hybrid coatings determined after 720 h does not exceed 0.002–0.01 wt% in all cases. Thus, the dry experimental condition in tests is close to the real application conditions of our hydrophobic hybrids.

To provide first a broad perspective, Materials Science and Engineering involves crystal structures [30], metals – including their mechanics [31], phase diagrams [32] and corrosion [33], as well as materials for saving energy [34], and petroleum [35] which is the source of synthetic polymers. Basic classes of materials include petroleum and other organic raw materials, ceramics, polymers, and composites [26]. The importance of

petroleum has been explained by Lucas and colleagues [35-39]. The role of polymers has been explained by Gedde and Hedenqvist [40].

Needless to say, there is a variety of polymers – and a large variety of their applications. Engineering polymers include polypropylene [41], a variety of poly-

ethylenes and poly(vinyl chloride). There are also polymers for specific uses. Thus, Taczała and colleagues developed poly(methyl methacrylate) reinforced with chemically modified cellulose microfibers for dental applications [42]. For reasons stated in the beginning, we focused on epoxies [43-50].

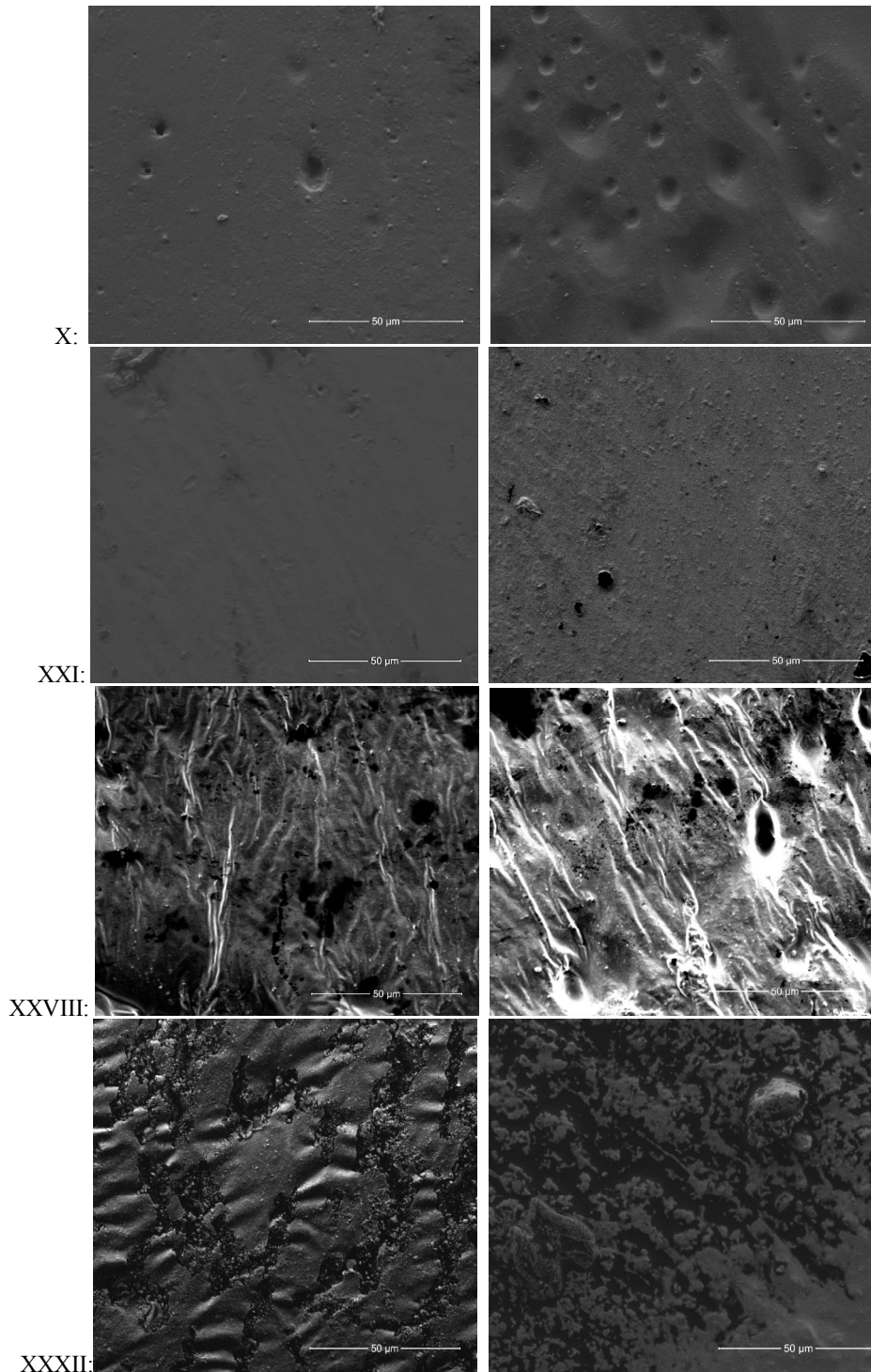


Fig. 5. SEM micrographs of polymer hybrids containing perfluoroalkyl methacrylic and epoxy side groups before and after tribology testing and thermal aging (50 µm)

4. Conclusions

In this work we have developed novel photostable, hydrophobic antimicrobial materials based on functionalized fluorine-organic methacrylate copolymers containing epoxy groups in the main chains. These materials have improved tribological characteristics: less wear, higher scratch resistance, appropriate viscosity, and acceptable dynamic friction. Our hybrids are characterized by high thermal stability and good adhesion to various substrates. They can be used for both short-term and long-term protection of cultural heritage and also as coatings for a variety of objects against a wide spectrum of biodestructors.

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АНТИБІОКОРОЗИВНІ ГІБРИДНІ МАТЕРІАЛИ ПІДВИЩЕНОЇ МІЦНОСТІ

Анотація. Одержані нові антикорозійні багатофункціональні гібридні матеріали на основі функційних перфторалкілметакрилатних кополімерів з епоксидними групами в основних ланцюгах та окремих біологічно активних сполук. Визначено, що гібриди є прозорими, демонструють непогану адгезію до різних поверхонь (пластик, дерево), високу в'язкоеластичну рекуперацію при випробуванні на подрятини, низькі показники зносу та температуру склування понад 323 К. За допомогою скануючої електронної мікрографії встановлено, що поділу фаз не відбувається. Підвищена механічна міцність і непогана стійкість до стирання є перевагами для використання синтезованих захисних та антикорозійних покриттів у різних сферах застосування, включаючи охорону культурної спадщини.

Ключові слова: гібридні матеріали, захисні покриття, антикорозійні покриття, перфторалкілметакрилати.